RESOLUTION A.685(17) adopted on 6 November 1991
WEATHER CRITERION FOR FISHING VESSELS OF 24 METRES IN LENGTH AND OVER
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THE ASSEMBLY,

RECALLING Article 15(j) of the Convention on the International Maritime Organization concerning the functions of the Assembly in relation to regulations and guidelines concerning maritime safety,

RECALLING ALSO resolution A.168(ES.IV) entitled "Recommendation on Intact Stability of Fishing Vessels",

NOTING that in resolution A.167(ES.IV) the Maritime Safety Committee had been requested to continue studies on improved stability criteria,

NOTING ALSO recommendation 1 of the International Conference on Safety of Fishing Vessels, 1977, regarding guidance on a method of calculation of the effect of severe wind and rolling in associated sea conditions contained in attachment 3 to the Final Act of the International Conference on Safety of Fishing Vessels, 1977,

RECOGNIZING the need to establish international standards for a weather criterion for fishing vessels of 24 metres in length and over,

HAVING CONSIDERED the recommendations made by the Maritime Safety Committee at its fifty-eighth session,

1. ADOPTS the Recommendation on Weather Criterion for Fishing Vessels of 24 metres in Length and Over set out in the annex to the present resolution;

2. NOTES that the weather criterion for fishing vessels of 45 metres in length and over, is identical to the criterion for these vessels, as contained in resolution A.562(14);

3. INVITES Governments to take steps to give effect to the annexed Recommendation as soon as possible, unless they are fully satisfied that their national stability requirements supported by long operating experience ensure adequate stability for particular types and sizes of fishing vessels;

4. RESOLVES that the weather criterion contained in the annex to the present resolution supersedes that contained in attachment 3 to the Final Act of the International Conference on Safety of Fishing Vessels, 1977.
ANNEX

RECOMMENDATION ON WEATHER CRITERION FOR FISHING VESSELS OF 24 METRES IN LENGTH AND OVER

1 SCOPE

1.1 The criterion given hereunder is recommended for new decked seagoing fishing vessels of 24 m in length and above and applies to all loading conditions.

1.2 This criterion supplements the stability criteria of the Recommendation on Intact Stability of Fishing Vessels in resolution A.168(ES.IV). The more stringent criteria of resolution A.168(ES.IV) and the weather criterion of the present Recommendation should govern the minimum requirements.

1.3 Administrations are invited to adopt, in conjunction with other appropriate criteria, the weather criterion of the present Recommendation unless satisfied that experience justifies departures therefrom.

2 RECOMMENDED CRITERION

2.1 The ability of a ship to withstand the combined effects of beam wind and rolling should be demonstrated as follows for each standard condition of loading, with reference to the figure:

.1 The ship is subjected to a steady wind pressure acting perpendicular to the ship's centreline which results in a steady wind heeling lever ($\ell_{w1}$).

.2 From the resultant angle of equilibrium ($\theta_0$), the ship is assumed to roll owing to wave action to an angle of roll ($\theta_1$) to windward. Attention should be paid to the effect of steady wind so that excessive resultant angles of heel are avoided*.

.3 The ship is then subjected to a gust wind pressure which results in a gust wind heeling lever ($\ell_{w2}$).

.4 Under these circumstances, area "b" should be equal to or greater than area "a".

.5 Free surface effects should be accounted for in the standard conditions of loading, e.g. according to appendix 1 to resolution A.168(ES.IV).

* The angle of heel under action of steady wind ($\theta_0$) should be limited to a certain angle to the satisfaction of the Administration. As a guide, 16° or 80% of the angle of deck edge immersion, whichever is less, is suggested.
The angles in the above figure are defined as follows:

\[ \theta_0 = \text{angle of heel under action of steady wind (see 2.1.2 and footnote)} \]

\[ \theta_1 = \text{angle of roll to windward due to wave action} \]

\[ \theta_2 = \text{angle of downflooding (} \theta_f \text{) or } 50^\circ \text{ or } \theta_C, \text{ whichever is less,} \]

where:

\[ \theta_f = \text{angle of heel at which openings in the hull, superstructures or deckhouses which cannot be closed weathertight immerse. In applying this criterion, small openings through which progressive flooding cannot take place need not be considered as open.} \]

\[ \theta_C = \text{angle of second intercept between wind heeling lever} w_2 \text{ and GZ curves.} \]
2.2 The wind heeling levers \( lw_1 \) and \( lw_2 \) referred to in 2.1.1 and 2.1.3 are constant values at all angles of inclination and should be calculated as follows:

\[
lw_1 = \frac{P \cdot A \cdot Z}{1000g} \text{ (m)} \quad \text{and} \quad lw_2 = 1.5lw_1 \text{ (m)}
\]

where: \( P = 504.2 \text{ N/m}^2 \) for fishing vessels of 45 m in length and over

For fishing vessels of 24 m in length and over but less than 45 m values of \( P \) should be taken from table 1.

Table 1

<table>
<thead>
<tr>
<th>( h ) (m)</th>
<th>1</th>
<th>2</th>
<th>3</th>
<th>4</th>
<th>5</th>
<th>6 and over</th>
</tr>
</thead>
<tbody>
<tr>
<td>( P ) (N/m(^2))</td>
<td>315.5</td>
<td>386.1</td>
<td>429.2</td>
<td>459.7</td>
<td>485</td>
<td>504.2</td>
</tr>
</tbody>
</table>

\( A \) = projected lateral area of the portion of the ship and deck cargo above the waterline (m\(^2\))

\( Z \) = vertical distance from the centre of \( A \) to the centre of the underwater lateral area or approximately to a point at one half the draught (m)

\( h \) = vertical distance from the centre of the projected lateral area of the ship above waterline to the waterline

\( \Delta \) = displacement (t)

\( g \) = 9.81 m/s\(^2\)

* The value of \( P \) used for ships in restricted service may be reduced subject to the approval of the Administration.
2.3 The angle of roll ($\theta_1$), referred to in 2.1.2, should be calculated as follows:

$$\theta_1 = 109kX_1X_2\sqrt{r.s} \text{ (degrees)}$$

where: $X_1 = \text{factor as shown in table 2}$

$X_2 = \text{factor as shown in table 3}$

$k = \text{factor as follows:}$

- $k = 1.0$ for a round-bilged ship having no bilge or bar keels;
- $k = 0.7$ for a ship having sharp bilges;
- $k = \text{as shown in table 4 for a ship having bilge keels, a bar keel or both}$

$r = 0.73 \pm 0.6 \text{ OG/d}$

with: $\text{OG} = \text{distance between the centre of gravity and the waterline (m) (+ if centre of gravity is above the waterline, - if it is below)}$

$d = \text{mean moulded draught of the ship (m)}$

$s = \text{factor as shown in table 5.}$

<table>
<thead>
<tr>
<th>Table 2</th>
<th>Values of factor $X_1$</th>
<th>Table 3</th>
<th>Values of factor $X_2$</th>
<th>Table 4</th>
<th>Values of factor $k$</th>
<th>Table 5</th>
<th>Values of factor $s$</th>
</tr>
</thead>
<tbody>
<tr>
<td>B/d</td>
<td>$X_1$</td>
<td>$C_b$</td>
<td>$X_2$</td>
<td>$A_k100$</td>
<td>$k$</td>
<td>$T$</td>
<td>$s$</td>
</tr>
<tr>
<td>---------</td>
<td>-------------------------</td>
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<td>------------------------</td>
<td>---------</td>
<td>----------------------</td>
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<td>--------------------</td>
</tr>
<tr>
<td>$\leq 2.4$</td>
<td>1.0</td>
<td>$\leq 0.45$</td>
<td>0.75</td>
<td>0</td>
<td>1.0</td>
<td>6</td>
<td>0.100</td>
</tr>
<tr>
<td>2.5</td>
<td>0.98</td>
<td>0.50</td>
<td>0.82</td>
<td>1.0</td>
<td>0.98</td>
<td>7</td>
<td>0.098</td>
</tr>
<tr>
<td>2.6</td>
<td>0.96</td>
<td>0.55</td>
<td>0.89</td>
<td>1.5</td>
<td>0.95</td>
<td>8</td>
<td>0.093</td>
</tr>
<tr>
<td>2.7</td>
<td>0.95</td>
<td>0.60</td>
<td>0.95</td>
<td>2.0</td>
<td>0.88</td>
<td>12</td>
<td>0.065</td>
</tr>
<tr>
<td>2.8</td>
<td>0.93</td>
<td>0.65</td>
<td>0.97</td>
<td>2.5</td>
<td>0.79</td>
<td>14</td>
<td>0.053</td>
</tr>
<tr>
<td>2.9</td>
<td>0.91</td>
<td>$\geq 0.70$</td>
<td>1.0</td>
<td>3.0</td>
<td>0.74</td>
<td>16</td>
<td>0.044</td>
</tr>
<tr>
<td>3.1</td>
<td>0.88</td>
<td>3.5</td>
<td>0.72</td>
<td>3.5</td>
<td>0.72</td>
<td>18</td>
<td>0.038</td>
</tr>
<tr>
<td>3.2</td>
<td>0.86</td>
<td>$\geq 4.0$</td>
<td>0.70</td>
<td>$\geq 20$</td>
<td>0.035</td>
<td></td>
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</tr>
<tr>
<td>3.3</td>
<td>0.84</td>
<td></td>
<td></td>
<td></td>
<td></td>
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<td></td>
</tr>
<tr>
<td>3.4</td>
<td>0.82</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>$\geq 3.5$</td>
<td>0.80</td>
<td></td>
<td></td>
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<td></td>
</tr>
</tbody>
</table>

(Intermediate values in tables 1 to 5 should be obtained by linear interpolation.)

* The angle of roll for ships provided with antirolling devices should be determined without taking into account the operation of these devices.
Rolling period $T = \frac{2C_B}{\sqrt{GM}}$ (seconds)

where: $C =$ rolling period factor* for $L < 45$ m

or $C = 0.373 + 0.023 \frac{B}{d} - 0.043 \frac{L}{100}$ for $L \geq 45$ m

The symbols in the above tables and formula for the rolling period are defined as follows:

- $L =$ waterline length of the ship (m)
- $B =$ moulded breadth of the ship (m)
- $d =$ mean moulded draught of the ship (m)
- $C_B =$ block coefficient
- $A_k =$ total overall area of bilge keels, or area of the lateral projection of the bar keel, or sum of these areas ($m^2$)
- $GM =$ metacentric height corrected for free surface effect (m).

* For fishing vessels less than 45 m in length, the "C" factor can be found in the "Code of Safety for Fishermen and Fishing Vessels - Part B". Furthermore, the "C" factor data for various types and loading conditions of smaller fishing vessels may be known by the Administration. For a specific fishing vessel, the "C" factor considered the most appropriate should be used.

For fishing vessels greater than or equal to 45 m in length, or if no "C" data are available or if they are considered inappropriate, then the equation for the "C" factor given in resolution A.562(14) should be used (see equation above).